



Attrition-Resistant Iron-Based Catalyst for F-T SBCRS

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Presenter Information

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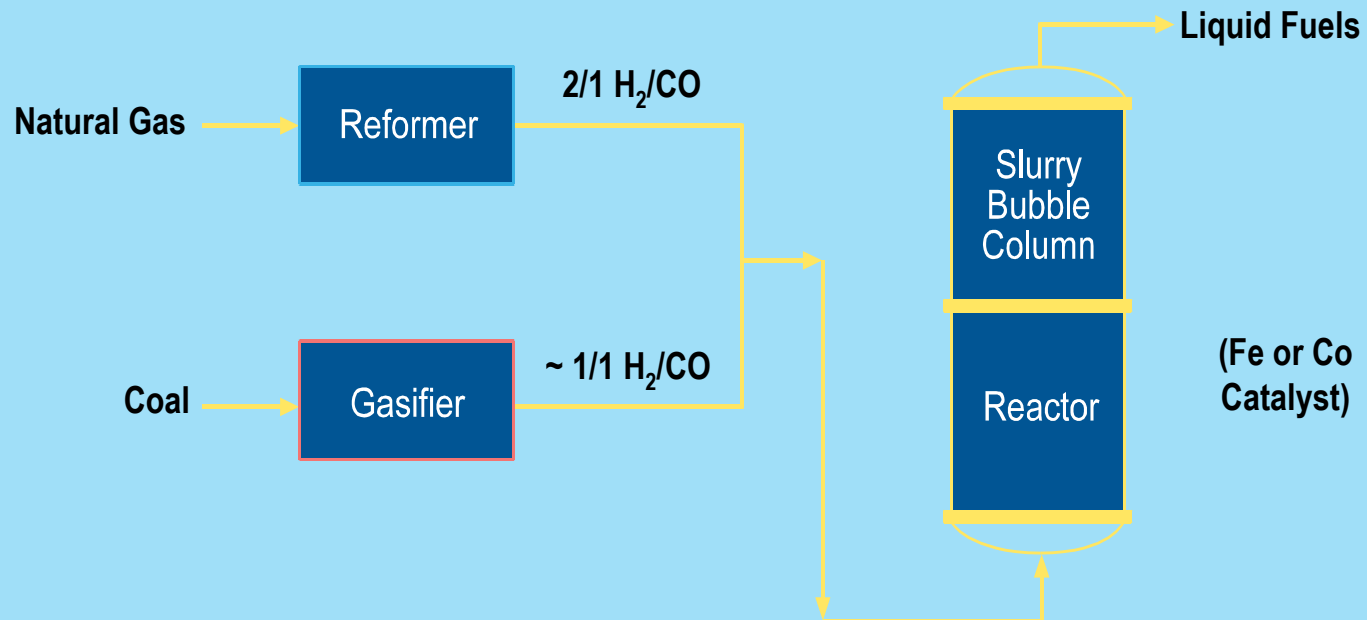
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Industrial Collaboration: Süd –Chemie, Inc.

Grant: DE-FG26-01NT41360

Performance Period: September 1, 2001-August 31, 2004

Background

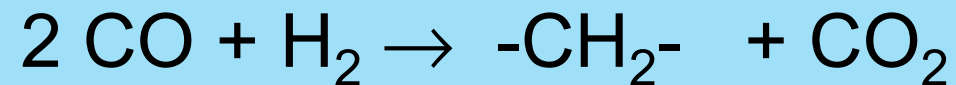
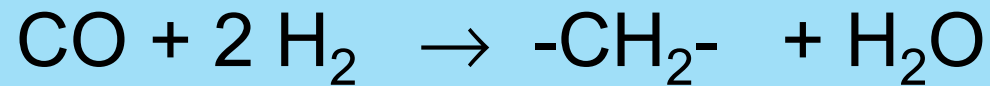


Objective

To develop robust iron-based Fischer-Tropsch catalysts that have suitable activity, selectivity and stability to be used in the slurry bubble column reactor.

- Improve the performance and preparation procedure of the high activity, high attrition resistant, high alpha iron-based catalyst synthesized at Hampton University;
- Seek improvements in the catalyst performance through variations in process conditions, pretreatment procedures and/or modifications in catalyst preparation steps and,
- Investigate the performance in a slurry reactor.

Reactions



Advantages of Iron Catalysts

- Inexpensive
- Specific activity for FT synthesis is high
- Water-gas shift activity
- Convert low H_2/CO ratio syngas

Advantages of Slurry Bubble Column Reactor

- Ability to remove heat and control reaction temperature
- High rate of reaction/productivity

Problem

- Attrition of the iron catalysts in fixed bed reactors
- Attrition of the iron catalysts in downstream filters in slurry bubble column reactors
- Leading to activity decline because of loss of catalyst from the reactors

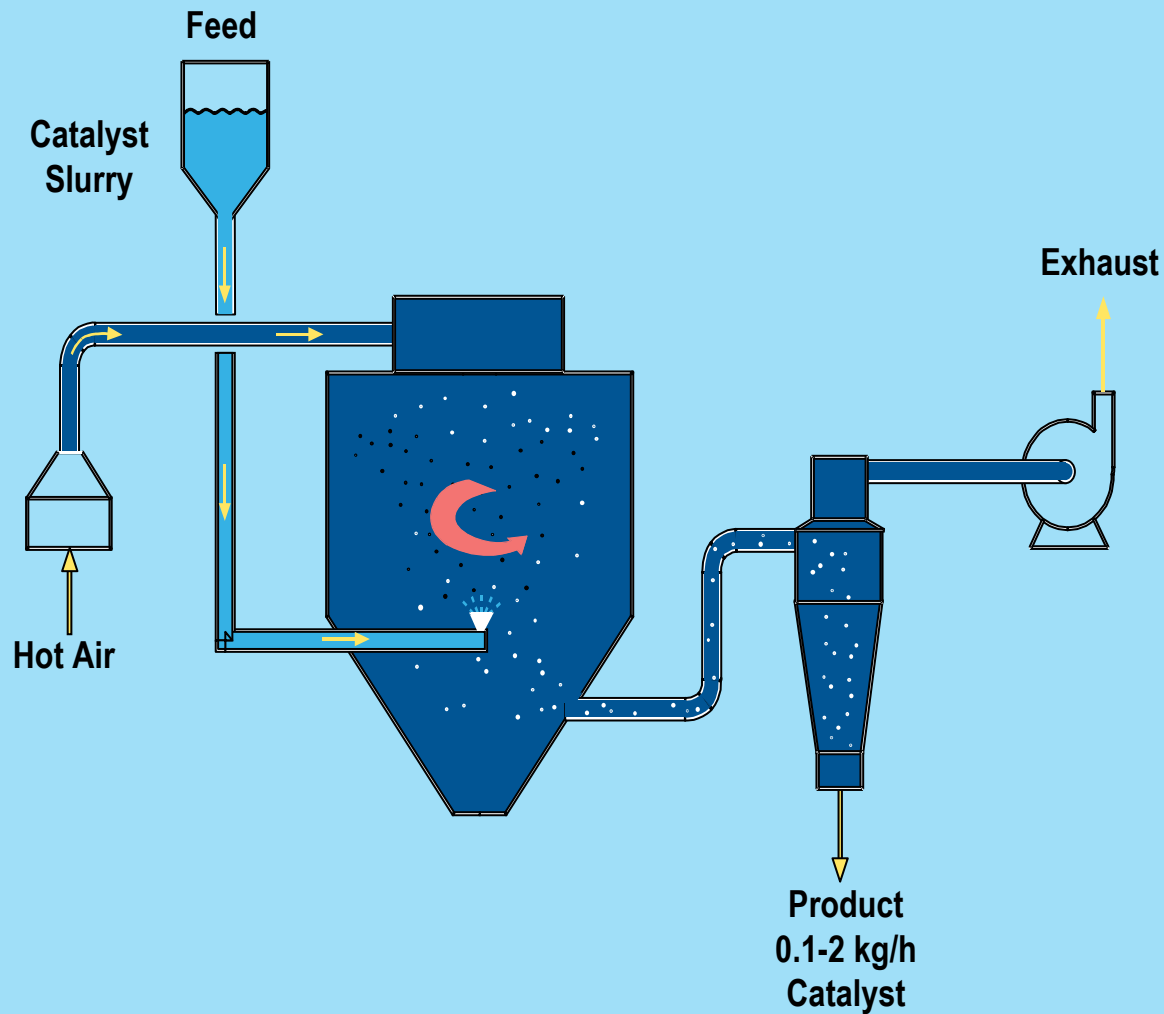
Remedy

To improve the physical strength of Fe FT catalysts, the spray-drying technique has been used for catalyst preparation without lowering catalyst activity

Catalyst Preparation

- Typical Fe FT catalysts is 100 Fe/5 Cu/4.2 K/x SiO₂
- Prepare a solution containing Fe(NO₃)₃• 9H₂O of appropriate concentration
- Prepare a solution containing CU (NO₃)₂ • 2.5 H₂O of appropriate concentration
- Take appropriate concentration of Si(OC₂H₅)₄
- Precipitation is carried using ammonium hydroxide (NH₄OH)
- Aqueous potassium in form of KHCO₃ is added to the slurry
- Slurry is spray dried at 250°C in Niro spray drier
- The spray dried catalyst is then calcined at 300°C for five hours in a muffle furnace
- The calcined catalysts were sieved between 38 and 90 µm

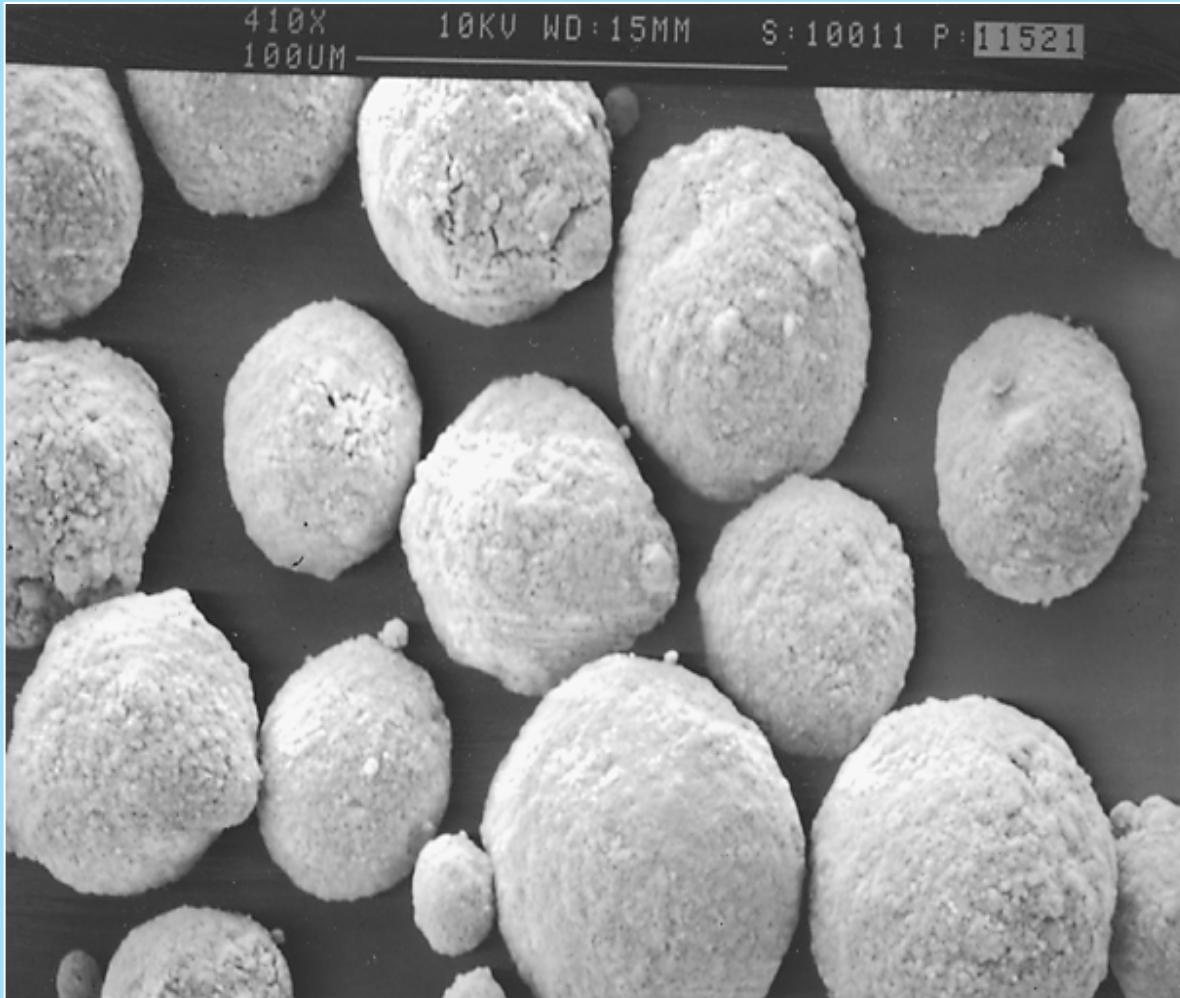
Niro Spray Drier



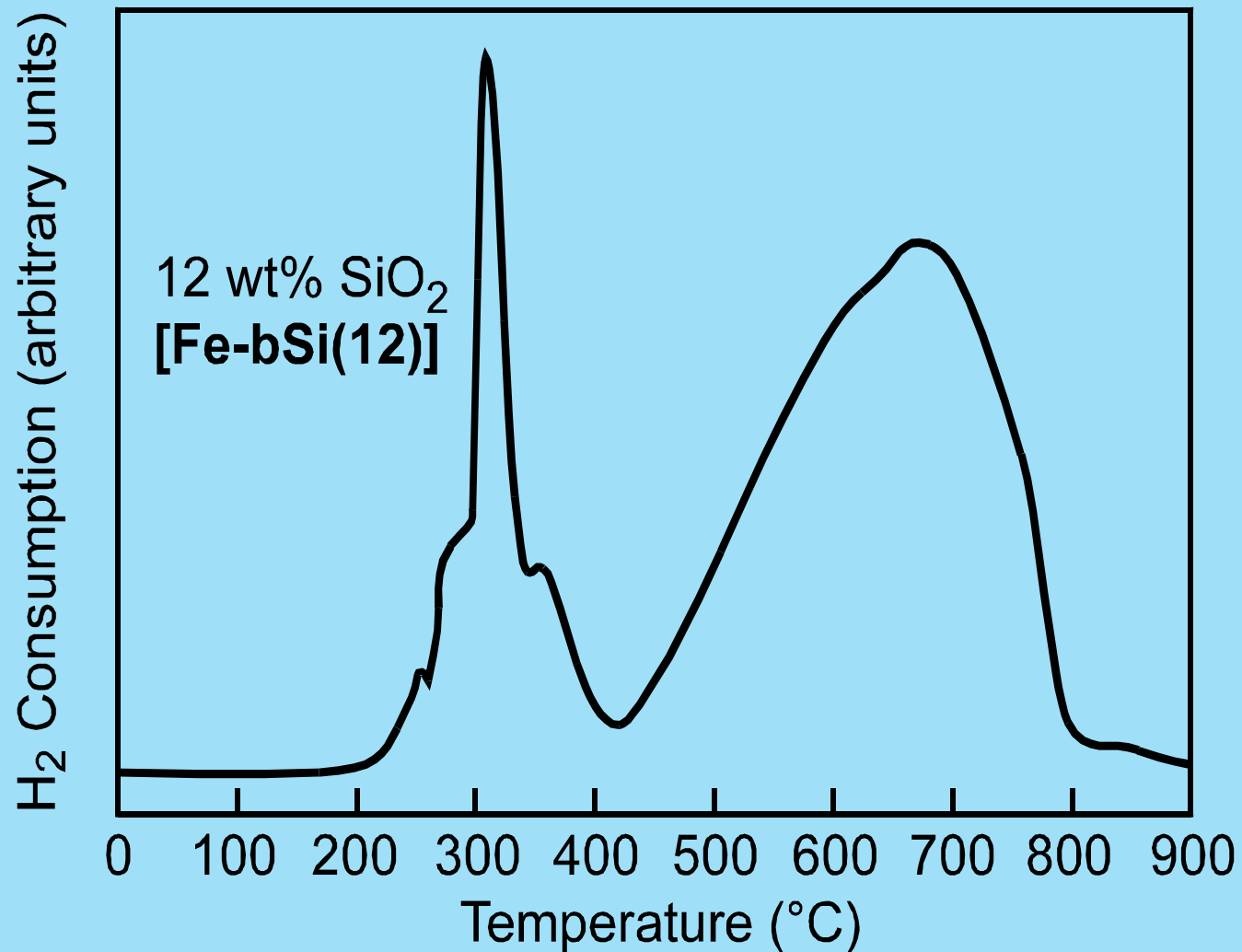
Catalyst Characterization Methods Employed

- BET
- Mercury porosimetry
- H₂-TPR
- SEM
- Metals analysis by AA
- Jet Cup

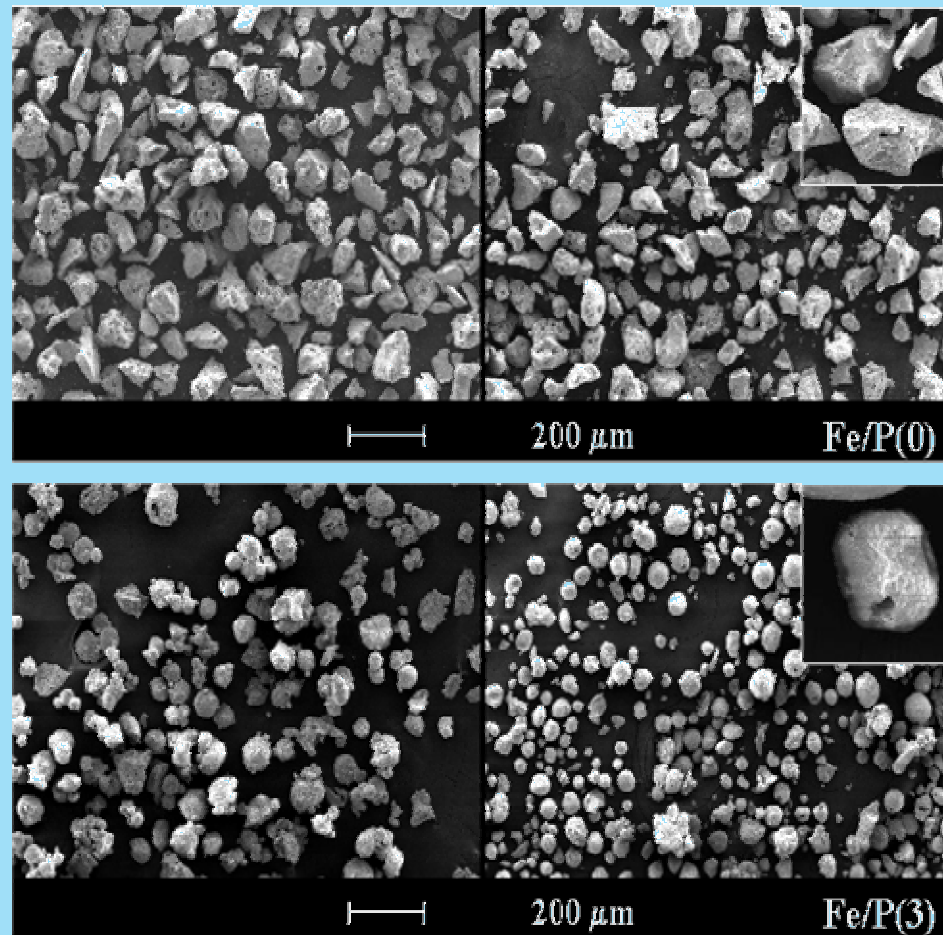
SEM Micrograph of Reduced Iron Catalyst



Hydrogen TPR of Iron Catalyst



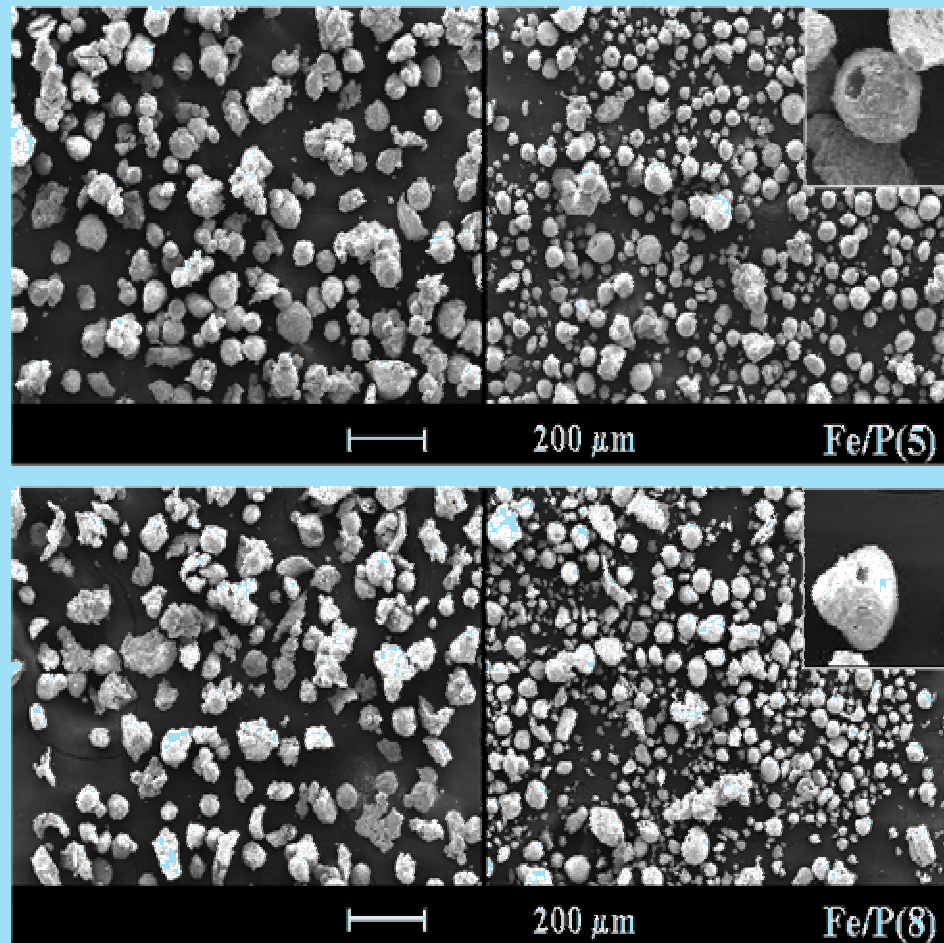
SEM Micrographs of Fe/P(0) and Fe/P(3) Before and After Attrition



Before Attrition

After Attrition

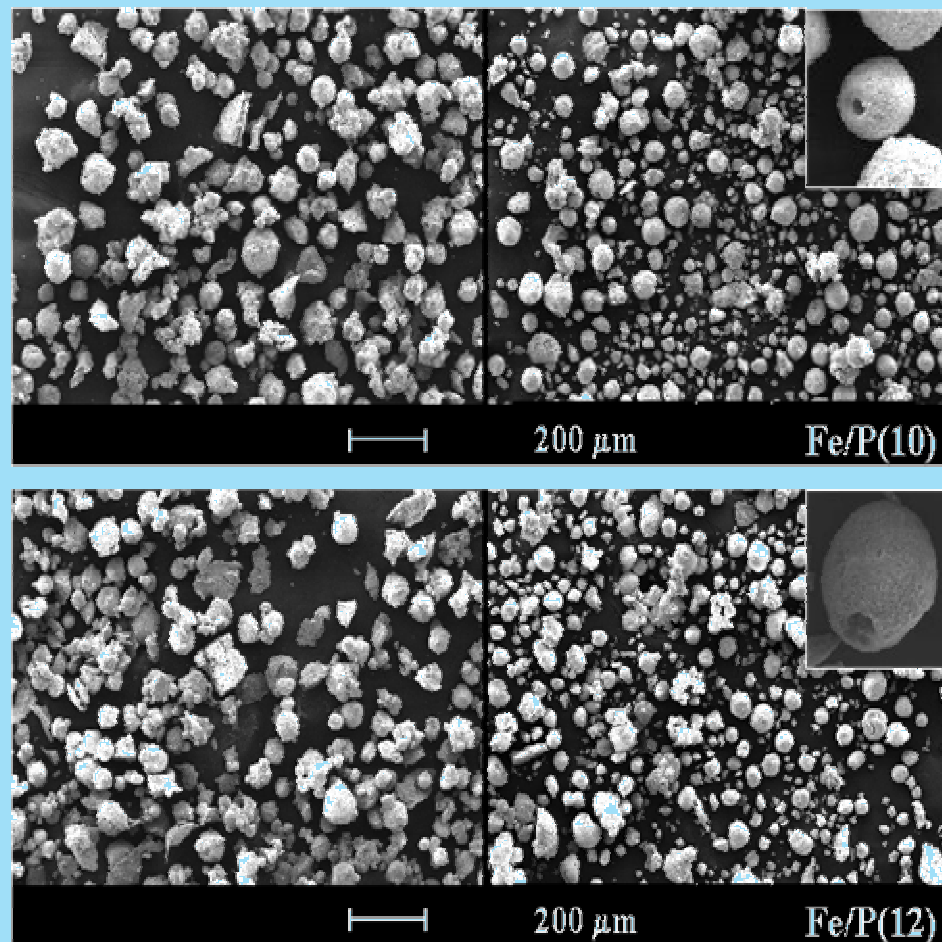
SEM Micrographs of Fe/P(5) and Fe/P(8) Before and After Attrition



Before Attrition

After Attrition

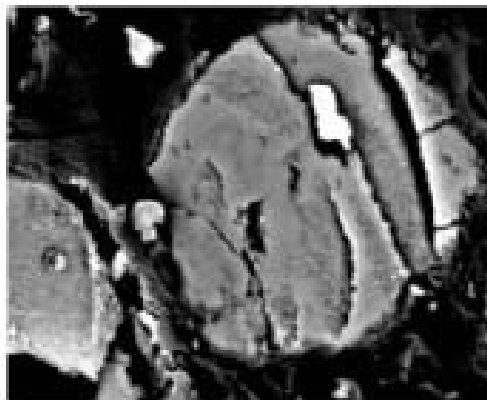
SEM Micrographs of Fe/P(10) and Fe/P(12) Before and After Attrition



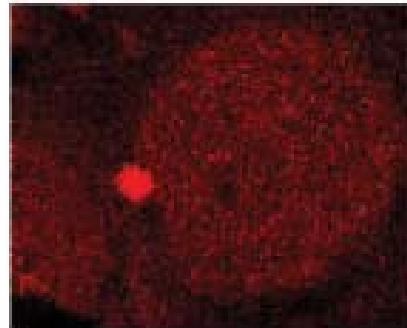
Before Attrition

After Attrition

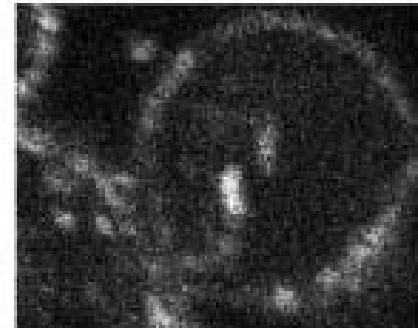
EDXS Results for the Cross Section of a Typical Fe/P(5) Particle



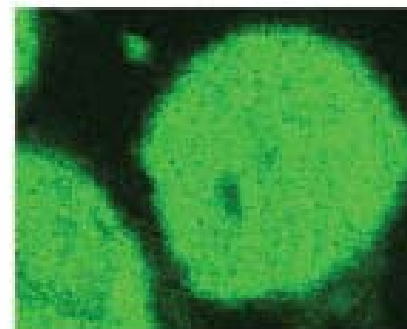
SEM Image of Fe/P(5) cross section



Si



K

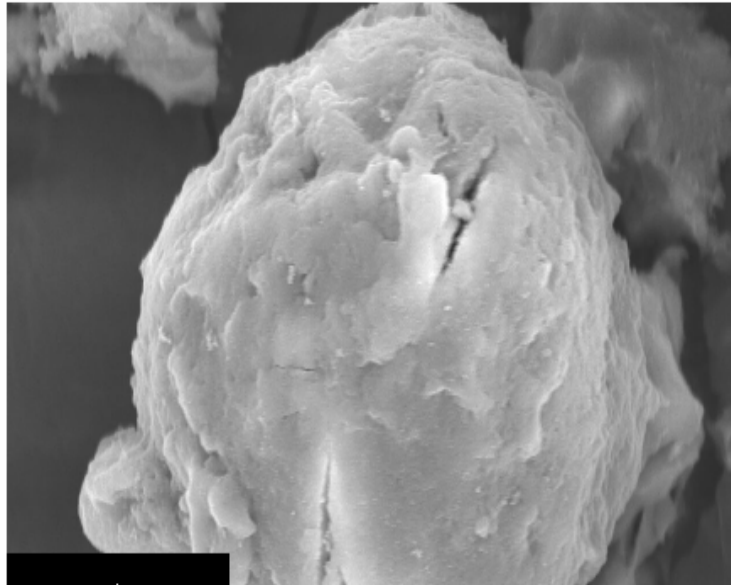


Fe



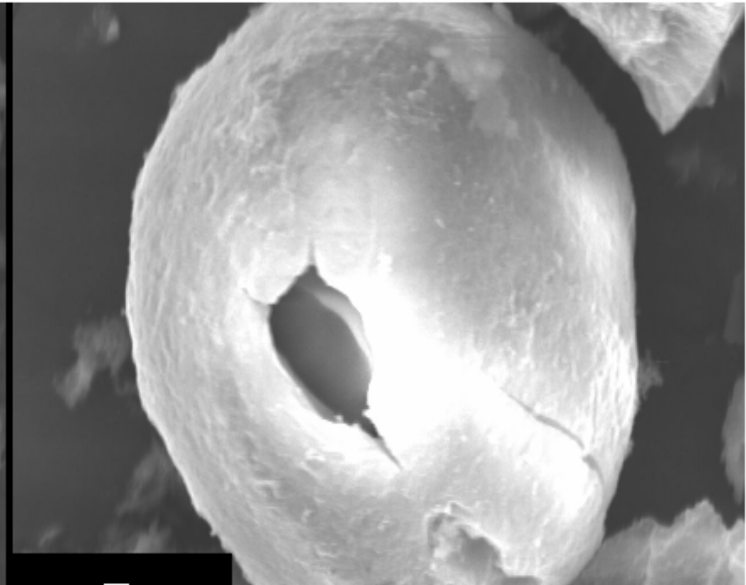
Cu

SEM Micrographs of Typical SiO_2 Structures After Acid Leaching [Fe/P(12)]



A

20 μm



B

10 μm

(A) Typical structure

(B) Particle with interior

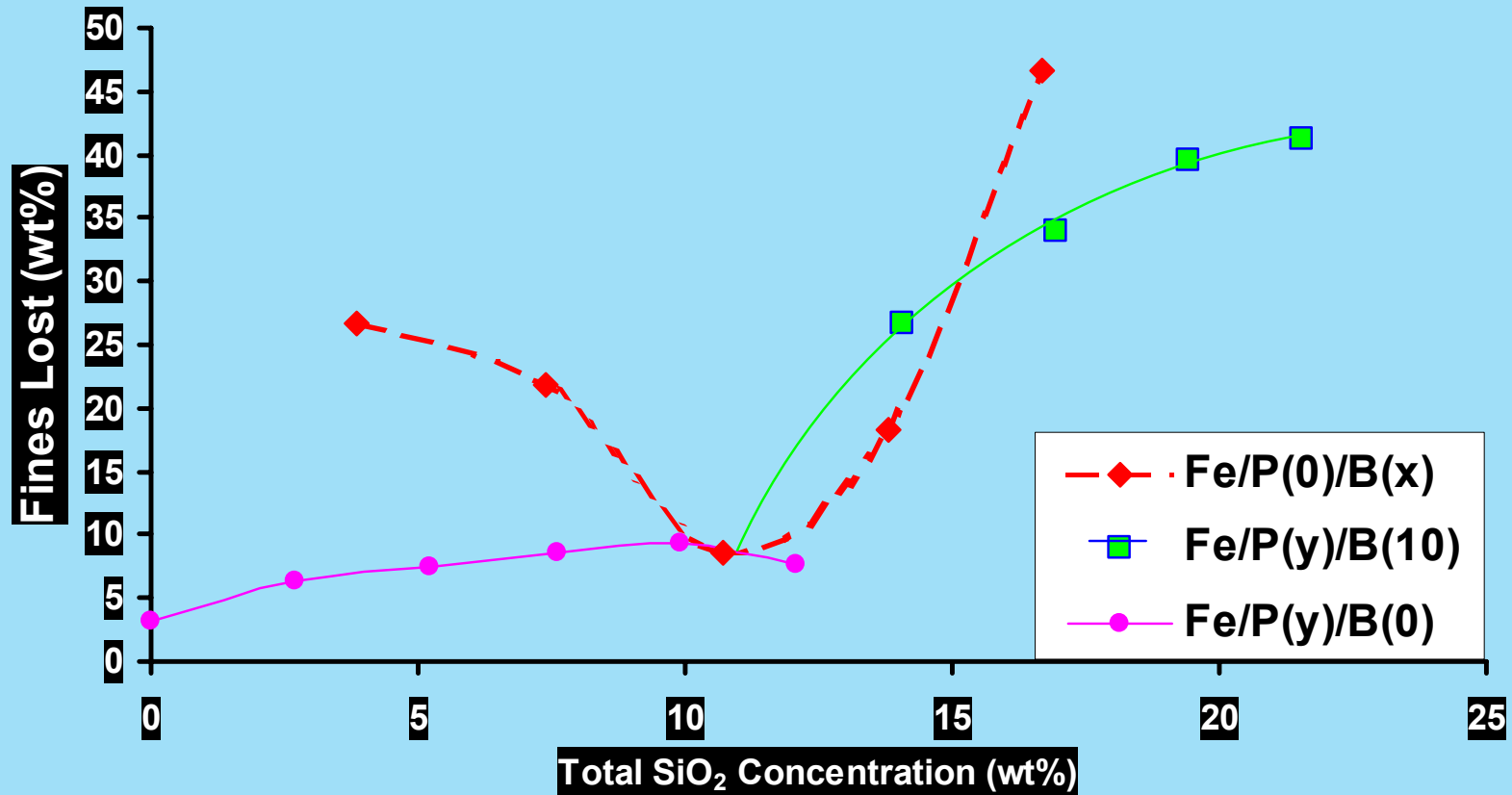
Jet Cup Attrition Test

- Attrition tests were conducted using a jet cup system
- In the jet cup test, 5g of each calcined catalyst sample was evaluated for attrition resistance under identical testing conditions using an air jet flow of 15 L/min with a relative humidity of $60 \pm 5\%$ at room temperature and atmospheric pressure
- After 1 hr. time-on-stream, the air jet flow was stopped, and the weight of fines collected by the downstream filter was determined
- The “weight percentage of fines lost” was calculated and used as one of the attrition indices
- The particle size distribution before and after attrition testing was determined with a Leeds & Northrup Microtrac laser particle size analyzer and used to calculate the “net change in volume moment”, the other attrition index used in our attrition studies. The volume moment is a measure of the average particle size.

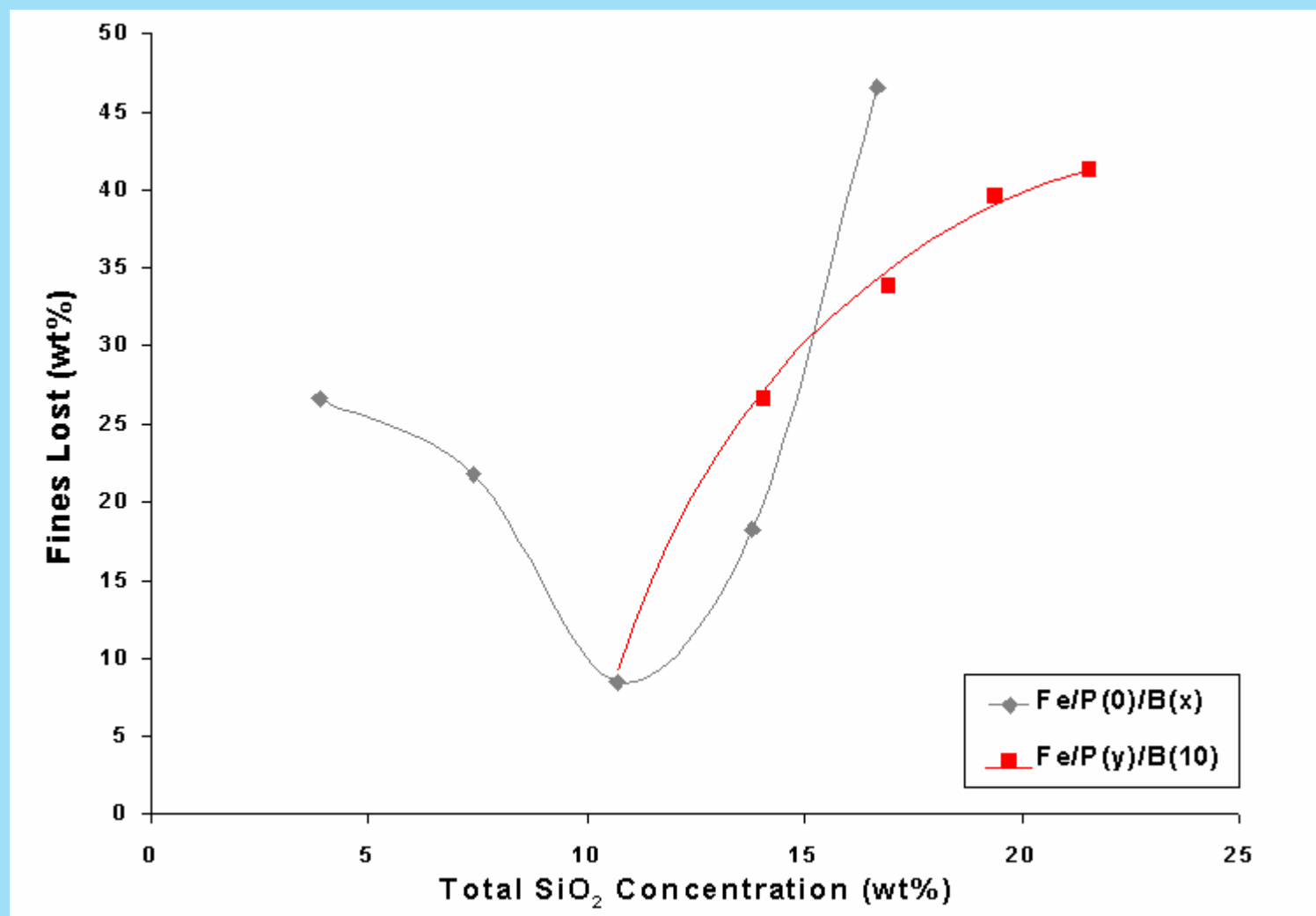
Jet cup attrition resistance test results

Catalysts	Attrition, wt %
Fresh (calcined)	4.8
CO pretreated	3.06
H ₂ /CO pretreated	3.85
H ₂ pretreated	4.02

Attrition Results (Jet Cup)



Attrition Test of Fe FT Catalysts

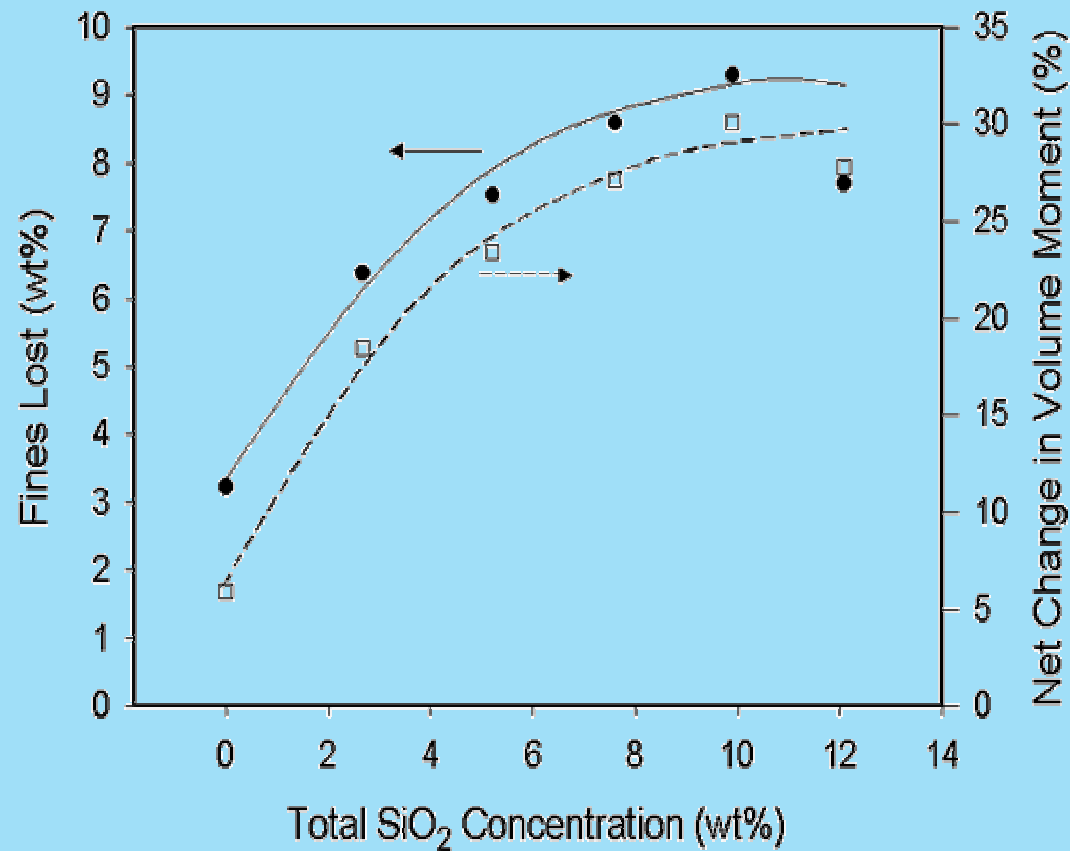


Jet Cup Attrition Results

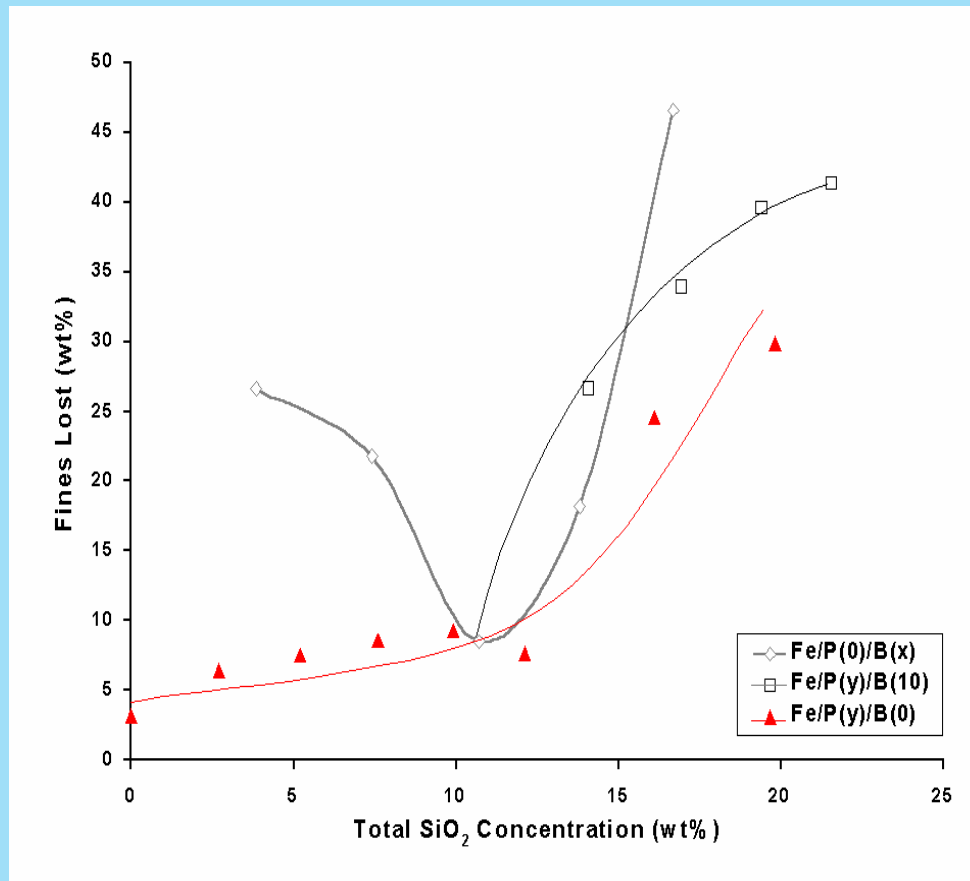
Catalyst	Total SiO ₂ Concentration (wt%)	Fines Lost (wt%) (a,b)	Net Change in Volume Moment (5) (c,d,e)
Fe/P(0)	0.0	3.2	6.0
Fe/P(3)	2.7	6.4	18.4
Fe/P(5)	5.2	7.5	23.4
Fe/P(8)	7.6	8.6	27.1
Fe/P(10)	9.9	9.3	30.1
Fe/P(12)	12.1	7.7	27.8
Fe/P(16)	16.1	24.5	---
Fe/P(20)	19.8	29.9	---

- (a) Wt% fines = weight of fines collected/weight of total catalyst recovered x 100%
- (b) Error = $\pm 10\%$ of the value measured.
- (c) Net change in volume moment was determined with reference to the particle size distribution before attrition testing.
- (d) Net change in volume moment (VM) = [(VM of sample after attrition test – VM of sample before test) / VM of sample before test] x 100%.
- (e) Error = $\pm 5\%$ of the value measured.

Jet Cup Attrition Results

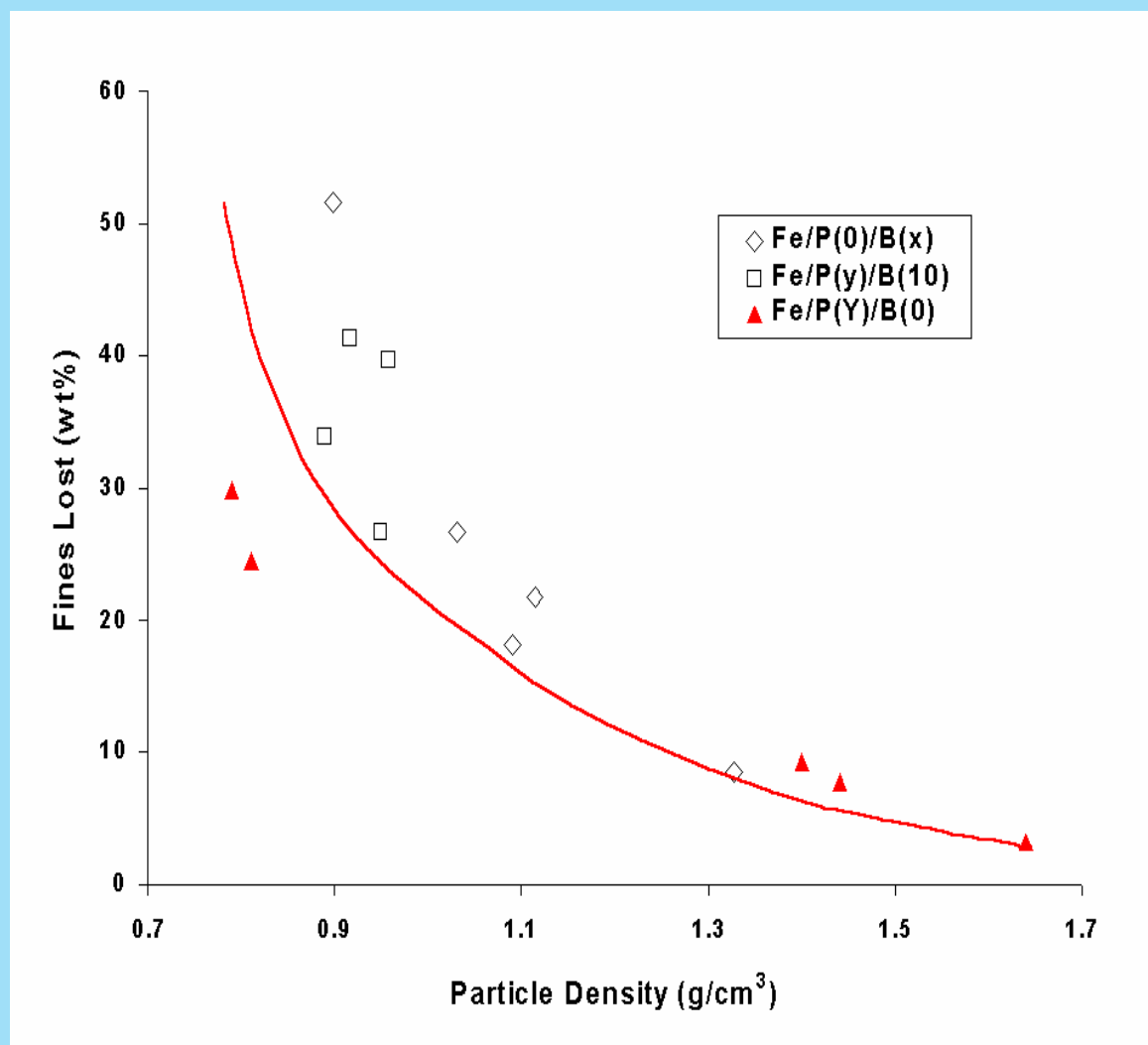


Weight Percentage of Fines Lost vs. Total Concentration of SiO_2 for Different Series of Spray-Dried Fe FT Catalysts



B refers to binder SiO_2 ; P refers to precipitated SiO_2 ; x and y refer to the amount of binder and precipitated SiO_2 added, respectively.

Weight Percentage of Fines Lost vs. Average Particle Density of Calcined Fe/P(y), Fe/B(x), and FE/P(y)/B(10) Catalysts



BET Surface Area and Pore Volume of the Iron Catalysts Studied

Table 2. BET Surface Area and Pore Volume of the Iron Catalysts Studied.

Catalyst	BET Surface Area (m ² /g) ^(a)		Pore Volume (cm ³ /g) ^(b)	
	Fresh	Attritted	Fresh	Attritted
Fe/P(0)	24	23	0.08	0.08
Fe/P(3)	69	63	0.12	0.11
Fe/P(5)	83	115	0.12	0.16
Fe/P(8)	48	69	0.11	0.14
Fe/P(10)	41	44	0.11	0.11
Fe/P(12)	76	84	0.11	0.12

(a) Error = $\pm 5\%$ of the value measured.

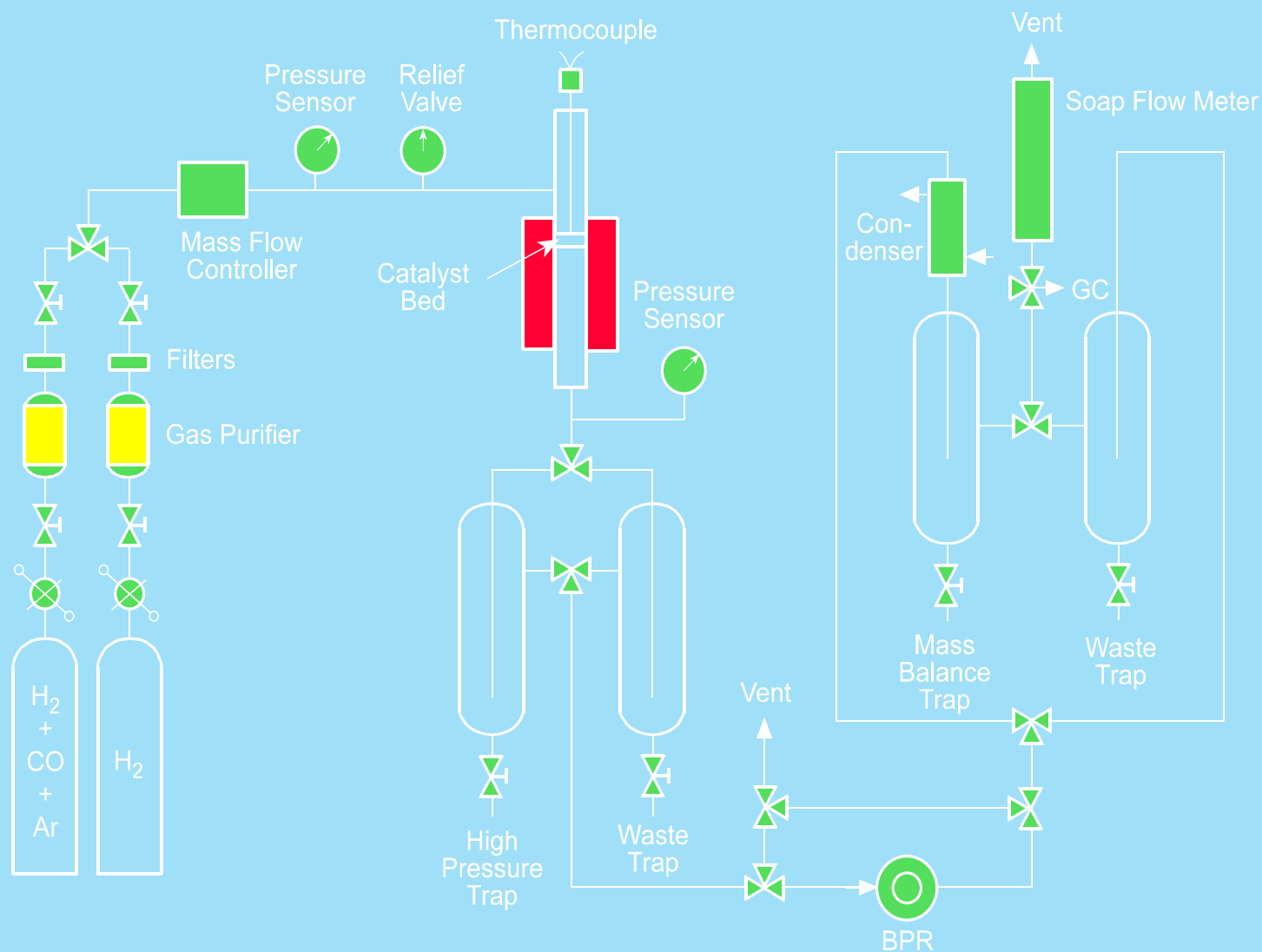
(b) Error $\equiv \pm 10\%$ of the value measured.

Macro Pore Volume and Particle Density of Selected Iron Catalysts

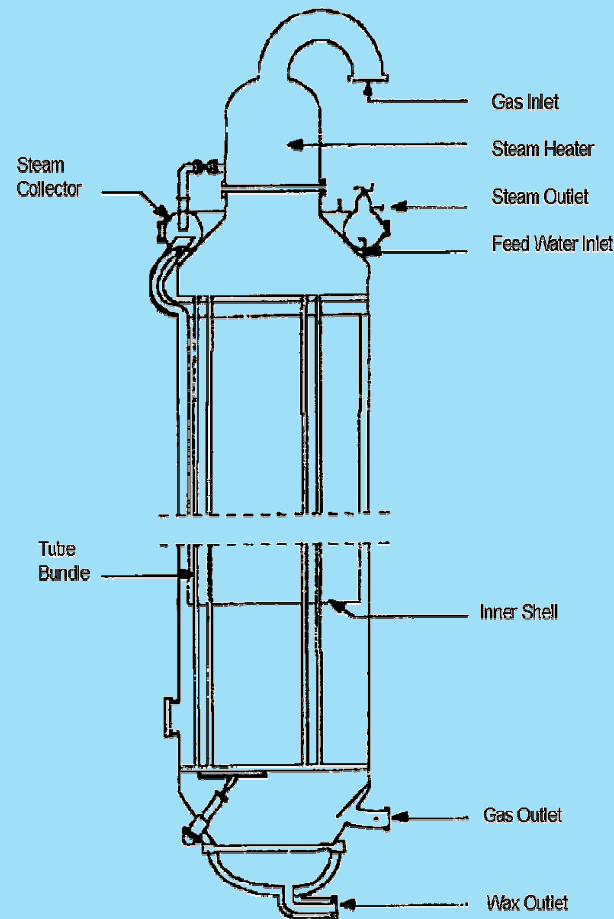
Catalyst	Macro Pore volume (cm ³ /g) ^(a)	Particle Density (g/cm ³) ^(b)
Fe/P(0)	0.25	1.64
Fe/P(10)	0.26	1.40
Fe/P(12)	0.24	1.44
Fe/P(16)	--	0.81
Fe/P(20)	--	0.79

- (a) Measured using mercury porosimetry, error $\equiv \pm 10\%$ of the valued measured.
- (b) Determined using low-pressure mercury displacement, error = $\pm 5\%$ of the value measured.

FT Reaction Fixed-Bed Test Apparatus



Tubular Fixed Bed (ARGE) Reactor



Experimental Conditions

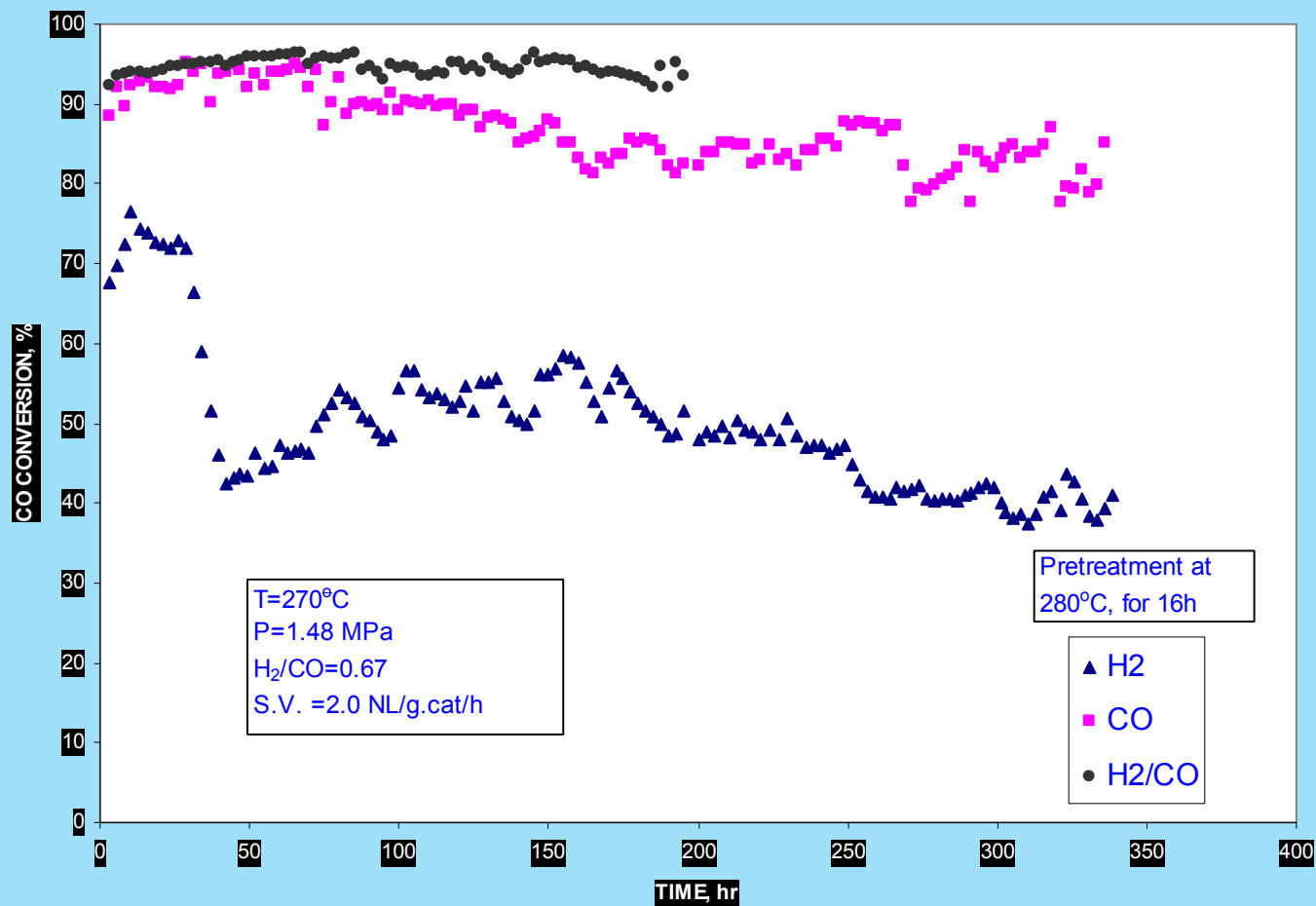
■ Activation

0.1 MPa, 280 °C, CO, H₂, CO+H₂, 16 h

■ Reaction

H ₂ /CO ratio	0.67/1
Space velocity	2.0 NL/g cat/h
Temperature	270 °C
Pressure	1.48 MPa

Variation of synthesis gas conversion with time on stream after different pretreatments



HU CSTR Set Up

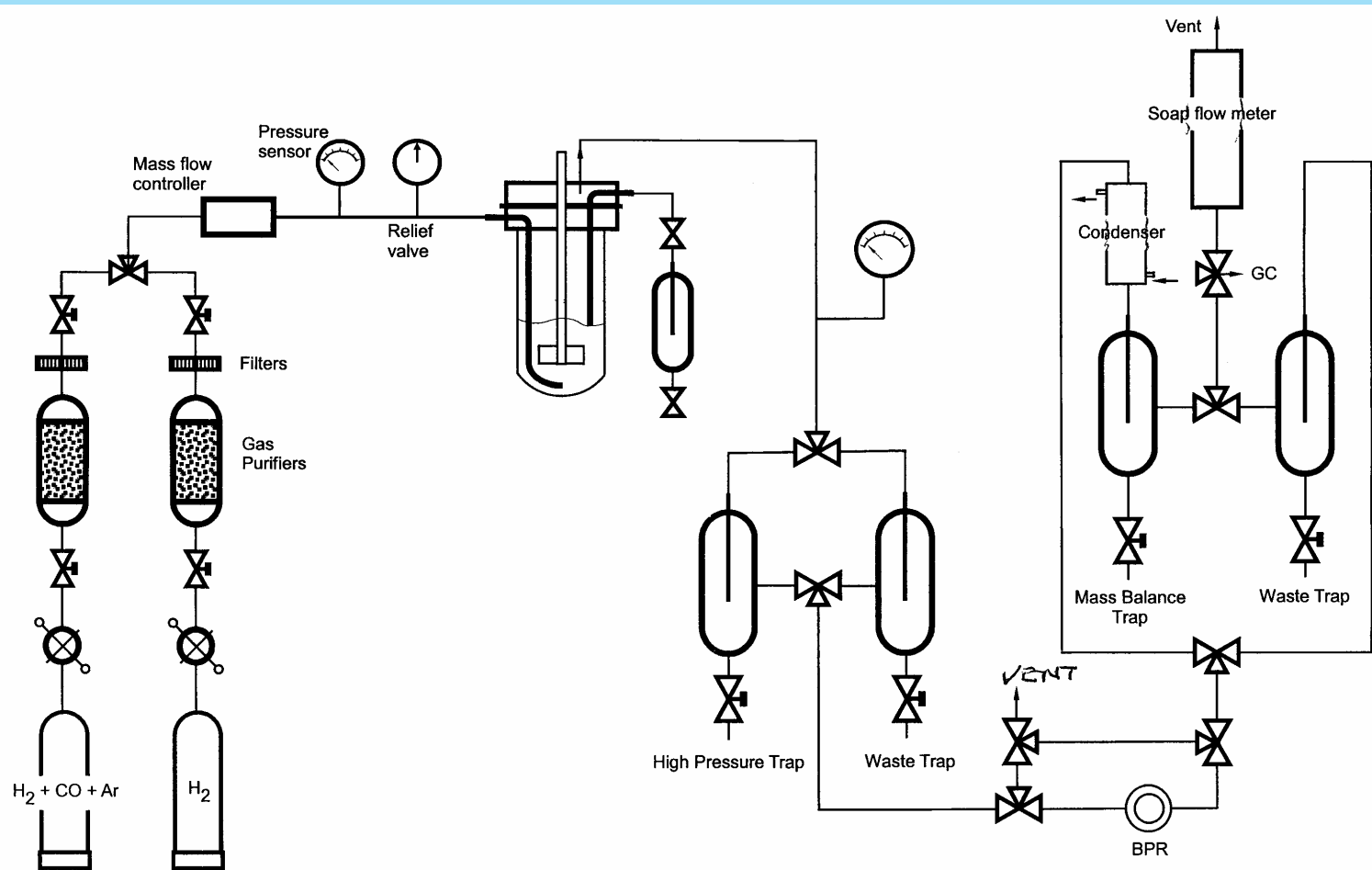
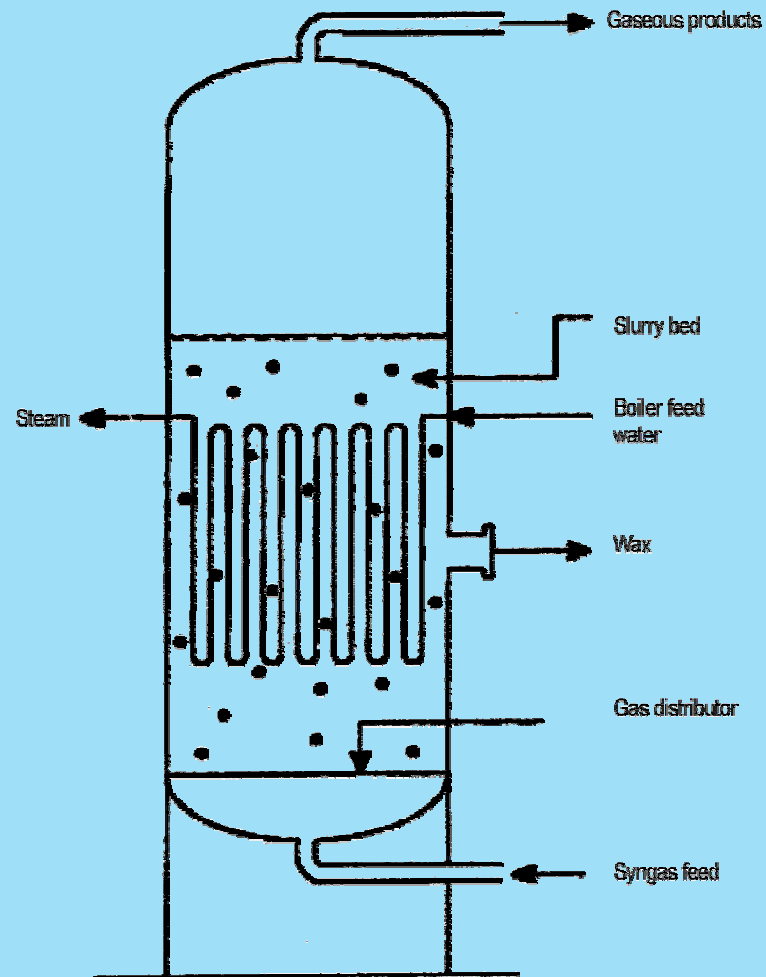


Figure 5. Schematic of Slurry F-T Reactor

Slurry Bubble Column Reactor



CSTR Experimental Condition

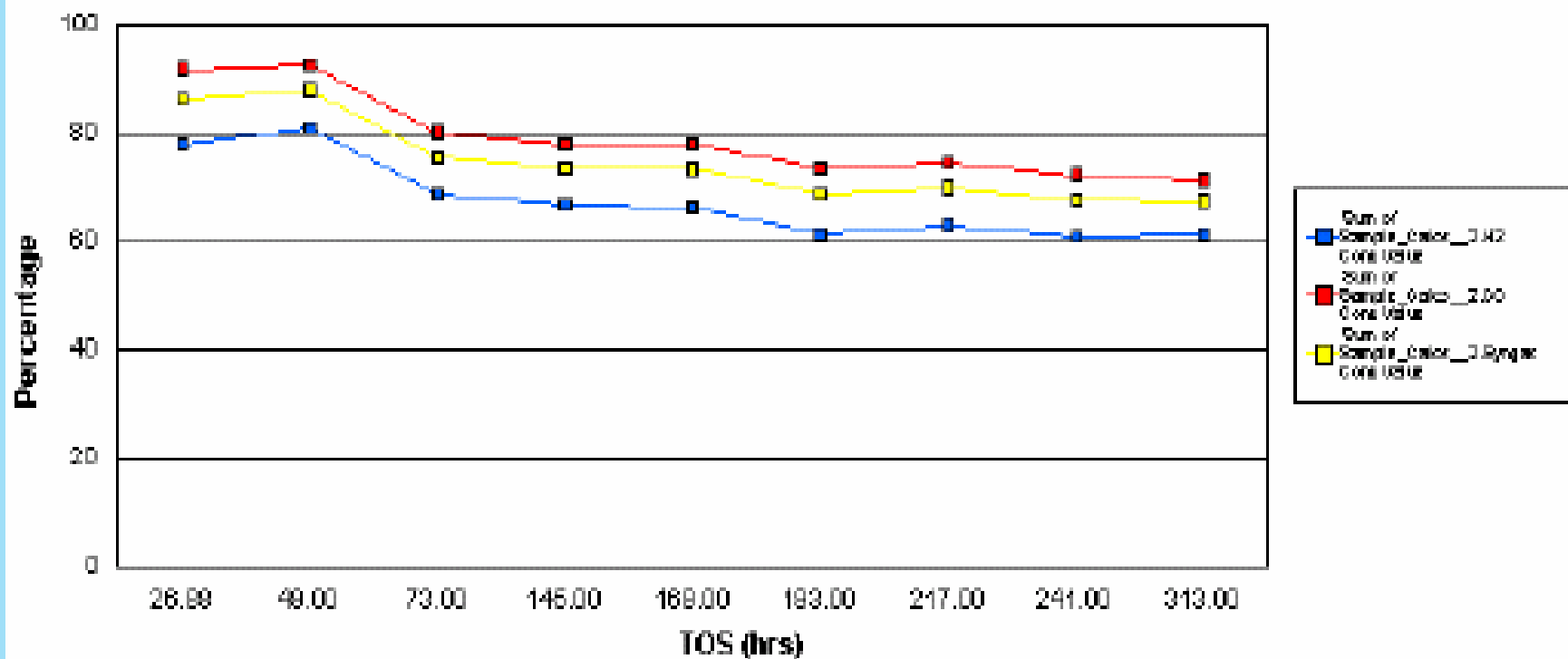
■ The conditions for testing are as follows:

CSTR Stirrer Speed (rev/min)	500
Temperature (°C)	260°C
Pressure (Mpa)	2.0
Space velocity (NL/gcat/h)	2.0
Syngas Composition	H ₂ /CO-0.67
Activation	0.1 Mpa, H ₂ /CO = 0.67, 280°C for 12 h

CSTR Results

Conversions

For BAO110



Summary

- Active iron catalysts prepared in 50+ gram quantities by spray drying
- CO conversion >95% achieved
- Silica content around 12 wt% showed the lowest attrition resistance
- The activity of the syngas ($H_2/CO = 0.67$) pretreated catalysts was the highest among all the pretreatment procedure used

Future Work

- Continue to improve catalyst performance
- Testing of the best catalysts in a CSTR

Acknowledgment

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